ATTACHMENT K

NOISE ANALYSIS

PRELIMINARY NOISE IMPACT ANALYSIS

Proposed

Lancaster Energy Facility #1
Lancaster, California

Prepared For

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Project #A10514

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1.0 EXECUTIVE SUMMARY

The proposed project will utilize four General Electric Frame 7B commercial, power generation systems. These systems use gas turbine engines, with auxiliary equipment, to produce 60 megawatts (MW) of electricity per unit, for a total power generation capacity of 240 MW. This generation system is intended for continuous online use. Development of this plant will provide additional power to the California electrical grid.

Without mitigation, onsite noise levels due to the proposed project would be in excess of allowable levels. The surrounding area will be impacted by the noise from the operation of this generating system. Based on this preliminary analysis, it is reasonable to conclude that, with the implementation of noise mitigation as described in this report, the noise from all sources in the proposed power generating facility can be reduced to levels that comply with the noise regulations of the City of Lancaster.

2.0 INTRODUCTION

This study is a preliminary noise impact analysis of the proposed Lancaster Energy Facility #1. The purpose of this study is to determine project feasibility and project requirements, including feasibility of mitigation.

The proposed location for this facility is near the northwestern corner of the intersection of Avenue H and Division Street. This subject site was selected because of its proximity to an existing power distribution substation and a natural gas main distribution line.

The proposed project will utilize four natural gas-fired General Electric Frame 7B commercial, packaged, power generation systems, as the basic unit for installation. The manufacturer's exhaust noise control system may not be utilized for two reasons: it provides insufficient noise attenuation, and the turbine exhaust will require additional emissions control systems.

For purposes of this study, the noise levels of the system(s) as a package, with the current exhaust noise levels, will be discussed. This system provides a known basis for planning the noise control system.

2.1 Project Description

The proposed project will utilize four General Electric Frame 7B commercial packaged power generation systems. These systems use gas turbine engines, with auxiliary equipment, to produce 60 MW of electricity per unit. The combined power output will be a nominal 240 MW.

The Frame 7B system includes a noise control housing for the turbine and generator systems.

Lancaster Energy Facility #1 will include a Dresser Waukesa 1,547 horsepower (Hp) auxiliary engine for plant start-up (in case of grid power failure), high pressure natural gas compressor(s) for the fuel system, auxiliary equipment for emissions control, several high volume air blowers, air conditioning, and electrical control systems.

2.2 General Site Characteristics

The subject property is semi-rectangular in shape and approximately four acres in area. The vacant site is adjacent to the north side of Avenue H and the west side of Division Street. The subject property is Parcel 4 of Tentative Parcel Map 26339, which is a 20-acre property.

The only nearby development within the city limits is to the northeast; this site houses a light industrial building and an occupied mobilehome. This is reportedly a caretaker's residence, and is the nearest residential property to the proposed project.

The area that is both east of Division Street and north of Avenue H is in the County of Los Angeles, but is not within of the City of Lancaster. This is across Division Street, immediately east of subject property.

Sensitive receptors nearby include a home to the northeast in the County of Los Angeles, at 239 Avenue G-8, a mobilehome located to the north near the site, single-family residences approximately one-third of a mile to the west, across Sierra Highway, and single-family residences on Avenue H-8, approximately one-half mile to the south.

2.3 Similar Site Investigation

As part of this analysis, we incorporated noise measurements from a similar power generation station in Escondido, California which uses a single LM6000-PC, 42 MW unit. This site is located on Tulip Street, just east of the I-15 freeway and one block north of Valley Parkway. Noise measurements were taken on Monday, May 15, 2000, at 6 p.m. (The facility was visited again recently, but no noise measurements could be taken because the facility was not in operation.) This facility is not contained in a building, but is shielded within a 20-foot high security control and noise wall.

Last year, access to the inside of the facility was not available; however, there was a gap in the wall next to a gate that allowed us to take overall noise measurements using a calibrated Type 1 sound level meter. At a distance of 15 feet outside the facility wall, a measurement of 57.3 decibels (dB(A)) was recorded. Through the gap in the gate, an inside measurement of 75.4 dB(A) was recorded.

3.0 ENVIRONMENTAL SETTING

3.1 Existing Noise Environment

This property is currently subject to noise from traffic on Avenue H and Division Street. To the west is Sierra Highway and the Union Pacific Railroad tracks approximately one-quarter mile to the east. The site is outside the 60 CNEL contour for the nearby Air Force Plant 42 airstrip.

Traffic noise measurements were not feasible due to strong winds during the site visits. Since the current traffic volume is low in comparison to projected traffic volumes (year 2020), only the impacts of future traffic will be addressed.

We conducted noise monitoring at four different locations on subject property, between Tuesday, May 1 and Saturday, May 5, 2001. The data are summarized in the attached spreadsheets.

3.2 Future Noise Environment

The future noise environment will include increased traffic noise from Avenue H, Division Street, Sierra Highway and the railroad, as well as noise generated from other commercial development on the adjacent parcels.

Projected traffic volumes were provided by Alan Perkins, Traffic Engineering Technician, City of Lancaster Public Works Department. According to the city's traffic model build-out for the year 2020, Avenue H between Division Street and Sierra Highway will have 7,700 westbound average daily trips (ADT) and 7,900 eastbound ADT. Using these figures, future traffic noise contours will be located at the following distances from the centerline of Avenue H: 70 dB, CNEL at 22 feet, 65 dB, CNEL at 70 feet, and 60 dB, CNEL at 198 feet. For more information, please refer to SOUND 32 Data and Results in the attachments.

Without significant new development, which is not currently foreseen, noise from the above transportation modes is not expected to increase the ambient noise level in the area by more than 3 to 5 dB.

Equipment

The following equipment was used during both the site investigation/ monitoring and the similar site investigation to measure existing noise levels:

- Larson Davis Integrating Sound Level Meter, Type I, Model 824, S/N 824A0343, with simultaneous 1/3 octave data analysis and FFT capability
- Larson Davis Integrating Sound Level Meters (2), Type I Model 820 S/N 0316 and S/N 0176, with data logging

- Larson Davis Model CAL200 Calibrator, S/N 0583
- Tripod, Tape Measure, Olympus Digital Camera

The sound level meters were calibrated immediately prior to and after use.

4.0 DEFINITIONS

- a. <u>A-Weighted Sound Levels</u>: Decibels (referenced to 20 microPascals), as measured with A-weighting network of standard sound level meter, abbreviated dB(A).
- b. <u>Background Noise</u>: Measured ambient noise level associated with all existing environmental, transportation, and community noise sources in the absence of any audible construction activity.
- c. <u>Construction Site</u>: For purposes of noise and vibration control requirements, the contract limits of construction. This includes Right-of-Way lines, property lines, construction Easement Boundary or property lines and Contractor staging areas outside the defined boundary lines, used expressly for construction.
- d. <u>Daytime</u>: The period from 6:30 a.m. to 10:00 p.m. Monday through Saturday.
- e. \underline{L}_{EQ} : Shall be defined as the equivalent sound level, or the continuous sound level that represents the same sound energy as the varying sound levels, over a specified monitoring period.
- f. \underline{L}_{MAX} : The RMS value of the period measurement peak noise level.
- g. <u>Community Noise Equivalent Level (CNEL)</u>: 24-hour average, where sound levels during the evening hours of 7 p.m. to 10 p.m. have an added 5 dB weighting, and sound levels during the night-time hours of 10 p.m. to 7 a.m. have an added 10 dB weighting (this is similar and often used interchangeably with L_{DN})
- h. Day-Night Sound Level (L_{DN}): A 24-hour average with 10 dB added weighting on the same night-time hours, but no added weighting on the evening hours.
- i. <u>Nighttime</u>: Periods other than daytime (as defined above), and including Sundays and legal holidays.
- j. <u>Noise</u>: Any audible sound which has the potential to annoy or disturb humans, or to cause an adverse psychological or physiological effect on humans.
- k. <u>Noise Level Measurements</u>: Unless otherwise indicated, the use of A-weighted and "slow" response of instrument complying with at least Type 2 requirements of latest revision of American National Standard Institute (ANSI) S1.4. Specification for Sound Level Meters.
- 1. <u>Noise-Sensitive Location</u>: Location where particular sensitivities to noise exist, such as residential areas, institutions, hospitals, parks, or other environmentally sensitive areas.
- m. Octave Filtered and 1/3 Octave Filtered Data: A contiguous series of continuous sound spectra centered about the stated frequency with half of the bandwidth above and half below the stated frequency. These data are used for machinery noise analysis and barrier effectiveness calculations.
- n. <u>Sound Transmission Class (STC)</u>: A single number rating calculated in accordance with

- ASTM E413 using values of sound transmission loss. It provides an estimate of the performance of a partition in certain common sound insulation problems.
- o. <u>Vibration</u>: Velocity in microinches per second. Vibration levels are expressed as velocity levels in decibels referenced to one microinch per second, abbreviated V_{dB} .
- p. __: The sound path length difference from direct line-of-sight from the source to the receiver and the indirect path over a barrier.

5.0 SYNOPSIS OF GOVERNING REGULATIONS

5.1 City of Lancaster Noise Element to the General Plan

4.3.1(d) When proposed projects include uses that could be potentially significant noise generators, require noise analysis to be prepared by an acoustical expert, including specific recommendations for mitigation when: 1) the project is located in close proximity to noise sensitive land uses or land which is planned for noise sensitive land uses, or 2) the proposed noise source could violate the noise provisions of the General Plan or Municipal Code.

4.3.1(h) Ensure that new commercial and industrial activities (including the placement of mechanical equipment) are designed so that maximum noise level standards at the property line of adjacent uses, thereby minimizing impacts on adjacent uses . . .

5.2 City of Lancaster Noise Ordinance

The following sections of the municipal code are cited:

8.24.040 Loud, unnecessary and unusual noises prohibited - Construction and building.

Except as otherwise provided in this chapter, a person at any time on Sunday or any day between the hours of eight p.m. and sunrise shall not perform any construction or repair work of any kind upon any building or structure or perform any earth excavating, filling or moving where any of the foregoing entails the use of any air compressors, jack hammer, power driven drill, riveting machine, excavator, diesel-powered truck, tractor, or other earth-moving equipment, hard hammers on steel or iron or any other machine tool, device or equipment which makes loud noises within five hundred (500) feet of an occupied dwelling, apartment, hotel, mobilehome, or any other place of residence.

17.16.220 - Subsection 18. Noise.

Uses which generate noise by the nature of their function and/or processes shall be required to demonstrate that the noise levels emitted from the use shall not exceed 65 dBA at any property line which abuts a commercial or residential zone or use.

5.3 County of Los Angeles Noise Ordinance

12.08.390 Exterior noise standards - Citations for violations authorized when.

A. Unless otherwise herein provided, the following exterior noise levels shall apply to all receptor properties within a designated noise zone:

	County of Los Angeles Noise Ordinance 12.08 390											
Noise Zone	Designated Noise Zone Land Use (Receptor Property)	Time Interval	Exterior Noise Level dB(A)									
I	Noise Sensitive Area	Anytime	45									
II	Residential Properties	10:00 p.m. to 7:00 a.m. (Nighttime) 7:00 a.m. to 10:00 p.m. (Daytime)	45 50									
III	Commercial Properties	10:00 p.m. to 7:00 a.m. (Nighttime) 7:00 a.m. to 10:00 p.m. (Daytime)	55 60									
IV	Industrial Properties	Anytime	70									

B. Unless otherwise herein provided no person shall operate or cause to be operated, any source of sound at any location within the unincorporated county, or allow the creation of any noise on property owned, leased, occupied or otherwise controlled by such person which causes the noise level, when measured on any other property either incorporated or unincorporated, to exceed any of the following noise standards.

Standard No. 1 shall be the exterior noise level which may not be exceeded for a cumulative period of more than 30 minutes in any hour. Standard No. 1 shall be the applicable noise level from subsection A of this section; or, if the ambient L_{50} exceeds the foregoing level, then the ambient L_{50} becomes the exterior noise level for Standard No. 1.

Standard No. 2 shall be the exterior noise level which may not be exceeded for a cumulative period of more than 15 minutes in any hour. Standard No. 2 shall be the applicable noise level from subsection A of this section plus 5 dB; or, if the ambient L_{25} exceeds the foregoing level, then the ambient L_{25} becomes the exterior noise level for Standard No. 2.

Standard No. 3 shall be the exterior noise level which may not be exceeded for a cumulative period of more than five minutes in any hour. Standard No. 3 shall be the applicable noise level

from subsection A of this section plus 20 dB; or, if the ambient $L_{8.3}$ exceeds the foregoing level, then the ambient $L_{8.3}$ becomes the exterior noise level for Standard No. 2.

Standard No. 4 shall be the exterior noise level which may not be exceeded for a cumulative period of more than one minute in any hour. Standard No. 4 shall be the applicable noise level from subsection A of this section plus 15 dB; or, if the ambient $L_{1.7}$ exceeds the foregoing level, then the ambient $L_{1.7}$ becomes the exterior noise level for Standard No. 4.

Standard No. 5 shall be the exterior noise level which may not be exceeded for any period of time. Standard No. 4 shall be the applicable noise level from subsection A of this section plus 20 dB; or, if the ambient L_0 exceeds the foregoing level, then the ambient L_{07} becomes the exterior noise level for Standard No. 4.

C. If the measurement location is on a boundary property between two different zones, the exterior noise level utilized in subsection B of this section to determine the exterior standard shall be the arithmetic mean of the exterior noise levels in subsection A of the subject zones. Except as provided in this subsection C, when an intruding noise source originates on an industrial property and is impacting another noise zone, the applicable exterior noise level as designated in subsection A, shall be the daytime exterior noise level for the subject receptor property.

5.4 Local Area Zoning

The site and all adjacent properties are zoned H1 for heavy industry. The nearby unincorporated area to the east is zoned D-2-1, which allows light industrial land use.

5.5 Site-Controlling Noise Regulations

The City of Lancaster Noise Ordinance requires that no noise source shall create noise levels which are above $65 \, dB(A)$ at the property line of any residential or commercial land use or zone. There is a residential property use to the northeast of the planned installation. Therefore, noise levels will be limited to $65 \, dB(A)$ at $400 \, feet$.

Note: While the City of Lancaster Noise Ordinance does not provide a noise limit for heavy industrial property, a reasonable property line standard common to many municipalities is 70 to 75 dB(A).

6.0 IMPACTS

Analysis Notes

To determine the combined noise levels when the noise level of two contributing sources are known, refer to Table 2; this equation is also valid when used successively for each additional noise source beyond the first two. The reverse procedure can be used to estimate the contribution

of one source, when the contribution of another concurrent source is known and the combined noise level is known. These methods can be used for L_{EQ} or for other metrics (such as L_{dn} or CNEL), provided that the same metric is used for all components.

Table 2. Sound Level Addition for Two Noise Sources									
Difference	Add to Higher Value								
0 - 1 dB	3 dB								
2 - 3 dB	2 dB								
4 - 9 dB	1 dB								
>10 dB	0 dB								

Noise data are typically supplied in two different formats: sound pressure and sound power.

The first format, sound pressure, is the level which would be heard or recorded by a sound level meter at a distance from a noise source. The second format, sound power, provides the basis for calculation of the sound pressure at a distance. The sound power format is the standard for presentation of data for heating, ventilating, and air conditioning equipment. The reader who is unfamiliar with data presented in this format should be aware that the sound power values appear to be significantly higher than the sound pressure values, because it includes all the sound emitted in all directions.

Information analyzed in this report is provided by the equipment manufacturers, and may have been provided in either format.

6.1 Potential Noise Sources

Noise sources associated with the proposed project can be classified into three categories:

- A. Construction noise
- B. Stationary mechanical equipment operation
 - a. Turbine engine air intake
 - b. Direct noise radiation from the turbine/generator enclosure
 - c. Turbine engine exhaust
 - d. Power failure start up engine
 - e. High pressure reciprocating natural gas compressor(s)
 - f. Absorption chillers and pumps

Note: This report does not address the numerous smaller noise sources such as ventilation blowers, air compressors, lube oil pumps, etc. The noise levels from these multiple smaller

units, while presenting the potential for significant noise impacts, is easily controlled pre and post installation with enclosures and small silencers.

C. Mobile noise sources, generally consisting of noise from cars and trucks

6.2 Description of Noise Sources

Construction noise

The attachment entitled "Construction Equipment Noise Levels" provides information on typical noise levels of construction activities. No extreme noise level generators (i.e., pile drivers or hoe rams) are anticipated for this construction.

Construction hours will be limited to the normal, allowable daytime hours stated in the City of Lancaster Noise Ordinance: 6:30 a.m. to 10:00 p.m., Monday through Saturday.

Therefore, construction noise will not be analyzed further.

Stationary mechanical equipment operation

The stationary mechanical equipment could produce noise levels of 85 to 90 dB(A) at the property line, if noise control mitigation measures are not included in the plant design.

The attached spreadsheet noted as S1 provides turbine octave noise data, unweighted overall noise data, and A-weighted noise data.

- A. The direct noise radiation from the turbine/generator enclosure (far-field) noise level is not available; this unit analysis is based on noise from a LM 6000 unit, which is 54.8 dB(A) at 400 feet or 68.8 dB(A) at 80 feet (approximate property line).
- B. The unsilenced turbine engine air intake (far-field) noise level is 109 dB(A) at 60 feet (approximate property line).
- C. The unsilenced turbine engine exhaust would produce approximately 107.6 dB(A) at 80 feet (approximate property line).
- D. The high-pressure reciprocating natural gas compressor is estimated to operate at 95 dB(A), at 3 feet from the unit.
- E. The absorption chillers and pumps have not yet been specified; therefore, actual data are not available. However, similar noise level units are routinely used in office and commercial construction, and the noise is typically controlled through use of a noise wall.

F. The power failure start up engine will not normally be used, but will be included for analysis purposes. Unsilenced exhaust from the engine will produce approximately 95.7 dB(A) at 75 feet; the engine noise will be approximately 95 dB(A) at 10 feet.

Mobile noise sources

Mobile noise sources, after construction is complete, will be minimal. Site access will be limited to normal operations, maintenance, and repairs vehicles. These operations and maintenance vehicles will contribute negligible overall noise to the area and will not be further addressed.

6.3 Impacts to Neighboring Areas

The General Electric Frame 7B commercial packaged power generation system, with the complete manufacturer's noise control package, would produce approximately 107.6 dB(A) at the property line. With the addition of the unmitigated noise produced by the high-pressure gas compressor(s) and chillers, the unmitigated property line noise level would be between 107.0 and 108.0 dB(A).

7.0 MITIGATION

Noise mitigation for this project would consist of three components:

- Equipment and Design Requirements
- Operational Requirements
- Procedural Requirements

7.1 Equipment and Design Requirements

The noise produced by this plant can be reduced to levels below the nearby residential property line limitation, 65.0 dB(A), through the implementation of the mitigation measures in the following section.

Portions of the project require special consideration for the noise mitigation systems. These include:

- A. The 900 degree (Fahrenheit) system exhaust. This will require silencing systems designed to ensure ongoing system functionality.
- B. The high-pressure natural gas compressor. Open air ventilation requirements are mandated by the State of California; these must be maintained by the noise quieting system.

Silencing for this system will utilize conventional techniques. The application of active noise cancellation was briefly explored as part of the overall noise control planning, but due to economic and reliability issues with current technology, it is not feasible for this project. The technique of active noise cancellation, through the use of computer-controlled generation of an inverted noise signal, is currently primarily used in smaller controlled situations, such as ventilation fan noise. It should be noted that both cost and reliability become an issue with active noise control applications as noise volumes increase.

The attached spreadsheets S2 and S3 provide the silencing details for the turbine and piston engine exhaust. A single silenced turbine property line noise level is expected to be 69.5 dB(A), which reduces to approximately 59.1 dB(A) at the nearest impacted residence. The noise level of three units at the residence would be approximately 63.9 dB(A) [the fourth turbine from any location will be distant enough to add only 0.1 to 0.2 dB(A)].

The high pressure natural gas pumps will need to be contained within a noise control enclosure to control their noise emissions. Without, specific octave noise data exact enclosure heights cannot be determined. However, there noise level should be reduced to less than 60 dB(A) with a noise control enclosure at least five feet above there highest point.

The power failure start-up engine exhaust will be mitigated to less than 60 dB(A) at 200 feet, and the engine will be contained within a building to control engine noise. Therefore, even though its use will be infrequent, it will maintain the required property line noise limits.

Note: All noise control enclosures should be made of either a manufactured noise shielding/ absorbing material or have noise absorbing material of at least three-inch thickness applied to the surface facing the noise source

7.2 Operational Requirements

The 65.0 dB(A) residential property line maximum level is a 24-hour requirement; therefore, no operational limitation requirements are anticipated.

7.3 Procedural Requirements

A. Attached is a data sheet from onsite monitoring performed prior to any project construction activities. The column headed "Towyard" is the towing yard on Avenue H-8 near the Paiute Intermediate School. The column headed "Trailer" is the commercial property with a mobilehome adjacent to the northeast comer of the project. The column headed "Grapevine" is a residence located at 239 Avenue G-8 (in the County of Los Angeles). The column headed "Brickwall" is the wall adjacent to the south side of Avenue H, west of 7th Street West.

The noise levels are significantly higher than might be ordinarily expected in this currently rural area. These high levels are attributed to extremely windy conditions during the monitoring period. It should be noted however, that these elevated noise levels are relevant to the area.

- B. Acoustical tests of the proposed plant will be completed as soon as practical, during and/or after the construction period. Additional noise control measures shall be implemented, if the measured sound levels at the residential property line exceed 65.0 dB(A). Noise monitoring procedures are as follows:
 - Acoustical consultant will utilize a Type I (Precision) or Type 2 (General Purpose) Sound Level Meter meeting the requirements of the latest revision of American National Standard Institute (ANSI) S1.4, Specification for Sound Level Meters.
 - Acoustical instruments will be field calibrated according to the manufacturer's specifications, prior to and following use. Calibrated sound level meters, microphones, and calibrators, with certified laboratory conformance per the manufactures specifications, will be used.
 - All measurements will use the A-weighting network and the SLOW response of the sound level meter, unless otherwise specified.
 - Impulsive or impact noises will be measured using the C-Weighting network and the FAST response of the sound level meter.
 - All measurement microphones will be fitted with an appropriate windscreen, and measurements will be taken at least six feet away from the nearest reflective surface.
 - Noise level measurement periods for intermittent noise shall be a minimum of 15 minutes.
 - If, in the estimation of the consultant, outside noise sources contribute significantly to the measured noise level, the measurements will be repeated with the same outside source contributions when construction is inactive to determine the background noise level.
 - Noise monitoring locations will be clearly identified on a drawing, and should include those locations where ambient noise measurements were conducted during this preliminary study. This monitoring should be conducted when the plant reaches 80% capacity.
- C. Final acoustical tests of the plant shall be conducted upon the completion of construction. If the noise level at the residential property line exceeds 65.0 dB(A), or any un-weighted octave bands exceed 80.0 dB, plant operations shall cease and the plant design shall be modified to achieve the required level of noise reduction. In this case, a new acoustical analysis shall be prepared.
- D. A Noise Monitoring Report shall be submitted to the City of Lancaster upon completion of the acoustical tests. The noise measurement reports shall include:

- Date, time, location and duration of measurement
- Instrument used
- Calibration information
- Sound level in dB(A) L_{EO}
- Notes
- Name and signature of acoustician
- E. All construction equipment should be maintained in good condition with factory-installed, or equivalent, noise control systems.

8.0 CONCLUSIONS

If the site is limited to a maximum nearby residential property line noise limit of 65.0 dB(A) $L_{\rm EQ}$, the current daytime average onsite noise level would increase from its approximately 55.0 dB(A) $L_{\rm EQ}$ from other outside sources to 65.0. dB(A) $L_{\rm EQ}$.

The Frame 7B units will require additional mitigation, beyond that provided by the manufacturer. However, the level of additional attenuation required may be achieved with implementation of conventional noise reduction techniques as part of the system's design.

With the implementation of noise mitigation, noise from all sources of the project can be controlled to levels in compliance with the noise regulations of the City of Lancaster. The local noise environment will receive only a moderate impact. However, the nearby residential use will experience noise levels in compliance with zoning, but higher than they are currently used to.

The similar facility in Escondido provides an example of how this type of facility can be built in compliance with the applicable noise regulations.

9.0 CERTIFICATION

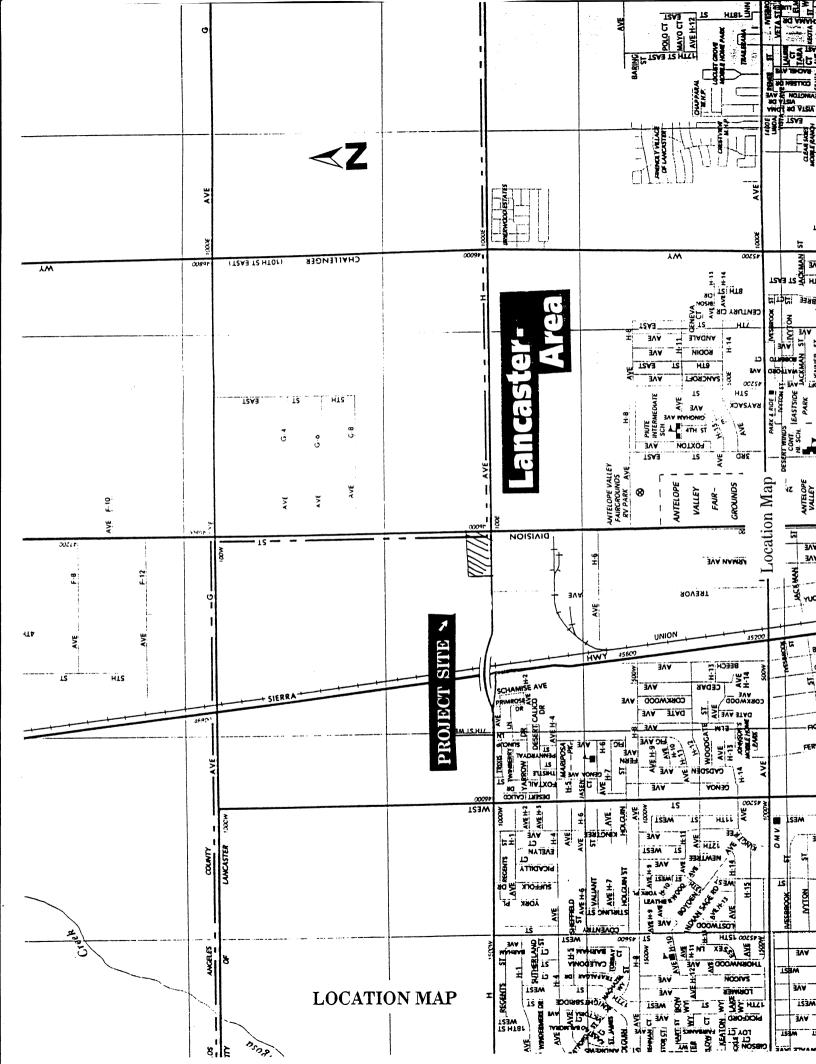
The findings and recommendations of this acoustical analysis report are a true and factual analysis of the potential environmental effects associated with the proposed development. This report was prepared by Charles Terry and Douglas K. Eilar.

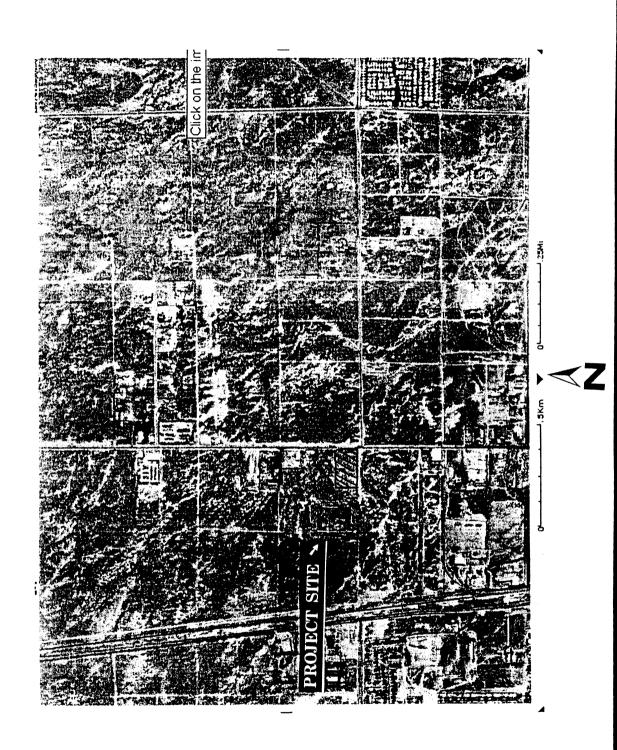
Sincerely,		
DOUGLAS EILAR & ASSOCIATES		
Charles Terry, Mechanical Engineer	Douglas K. Eilar	
Consultant in Acoustics, Investigator	Principal	

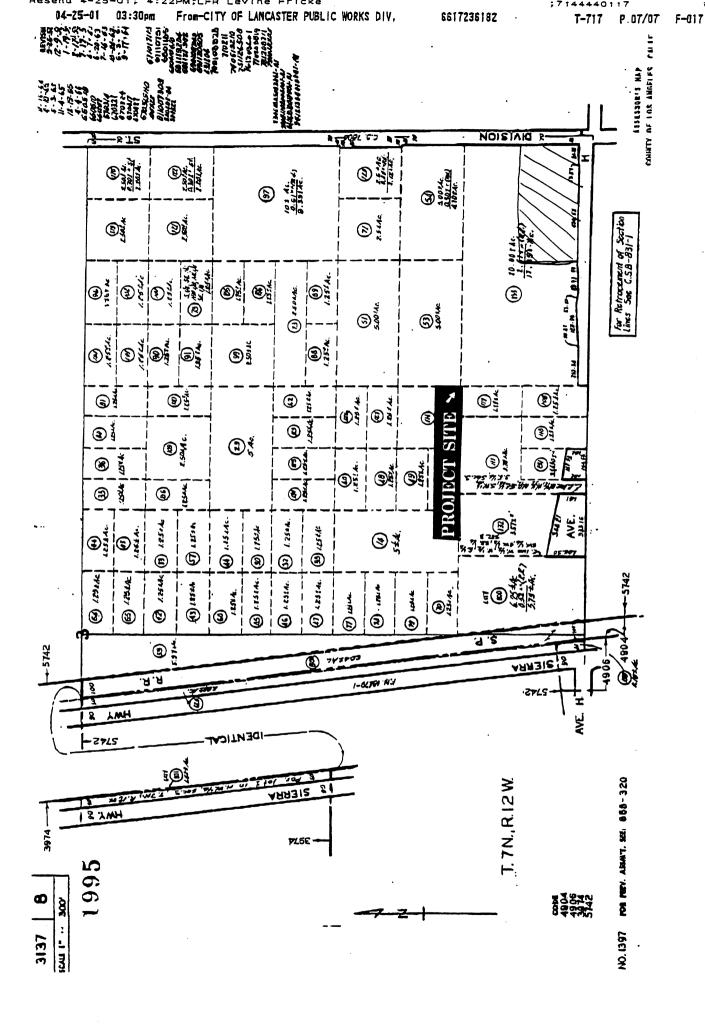
CT:elm

10.0 REFERENCES

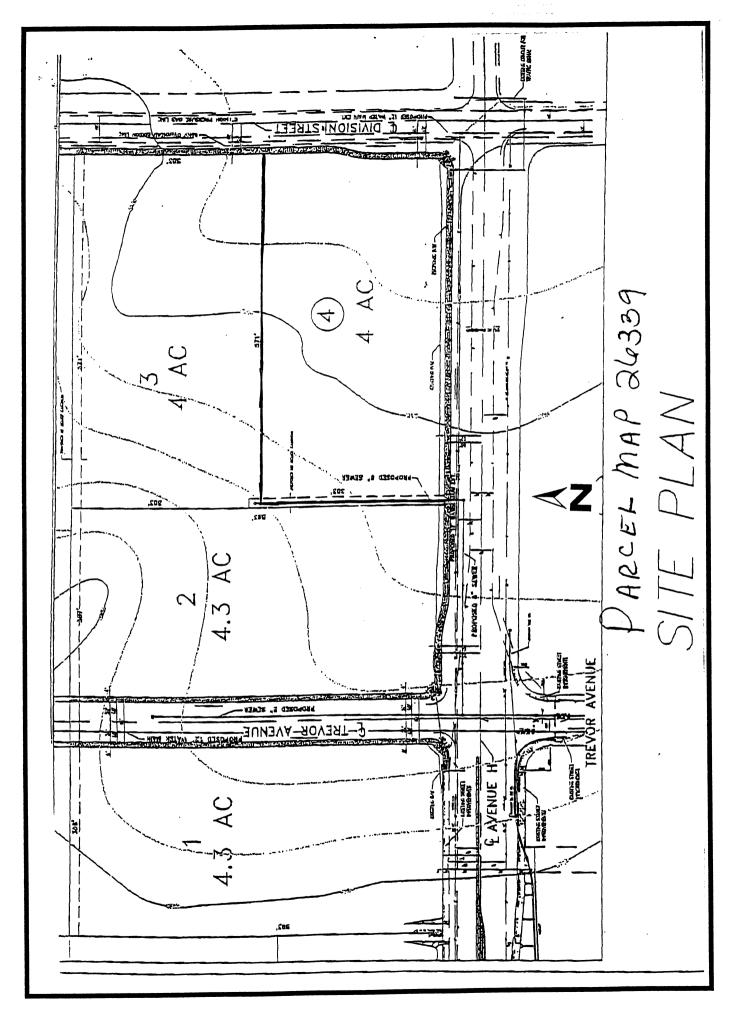
- 1. City of Lancaster Noise Ordinance
- 2. City of Lancaster Noise Element to the General Plan
- 3. County of Los Angeles Noise Ordinance

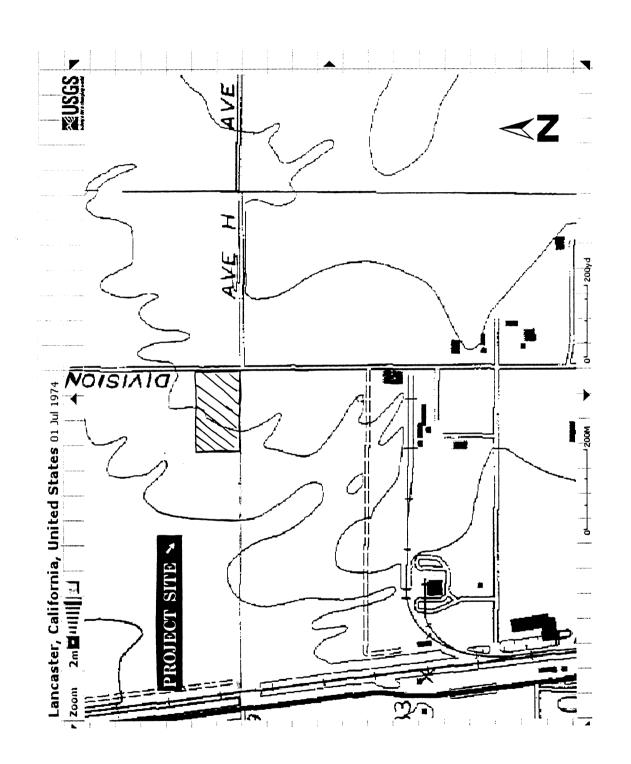






ASSESSOR'S MAP





A GE Power Systems Business	Customer: Description:	LM6000 Turb	ine Generator S	ound Pow	er Levels	•	
16415 Jacintoport Blvd.	Project:						
Houston, TX 77015	Date:	18 OCTOBER	R 2000				
Unsilenced, In-duct Sound Power Levels for the L	LM6000 Turbine Exhaus	: at Diffuser	Flange.				
SOUND POWER LEVELS OF THE LM6000 Turbine Com	nbustion Exhaust.						
	Octave Band Center	Frequency (Hz))				
Item Description 31.5	63 125 250 500	1K 2K	4K 8K	Lin.	A-Wt.		
So	und Power Levels (PWL's	i) in dB re 10 ⁻¹²	Watts				
UNSILENCED COMBUSTION EXHAUST In-Duct Sound Power Levels at the Turbine Diffuser Flange PWL: LM6000-PC Exhaust at FULL-LOAD 137 (Stack Directivity Not Included) NOTE: The above figures are what we use to repres exhaust duct. The low-frequency numbers are some silencer at the stack base, for our typical standard BF is included in the above figures. Stack end reflection	138 137 140 137 ent PWL's "at the diffuse what elevated, to inclue s RADEN 45' exhaust stack	126 122 r flange", inside elf-generated resolution of the state of the	120 109 e the turbine noise of the flection loss	145.1	136.7	<	NOTE: 1 st
DIL: DIL - Stack End Reflection Loss (dB) 6 (Subtract these values from the above figures to see	3 1 0 0	0 0	0 0				
PWL: LM6000-PC Exhaust at FULL-LOAD 124 (according to the GE Installation Design Manual) NOTE: These figures are lower in the low-frequency turbulence at the combustion exhaust exit, plus it may They also do not state if these figures are in-duct (i.e.	y already include end refle	ection losses.		147.8	143.9		

GE Aero Energy Products A GE Power Systems Busine 16415 Jacintoport Blvd. Houston, TX 77015

CUSTOMER PROJECT DESCRIPTION PROJECT NUMBER

LM6000 Std. Package - 90 dBA 6 OCTOBER 2000

RE: Noise Model, for ONE (1) Standard LM6000-PC Package, 60-Hz.

- Main Turbine Generator Unit Only, with STANDARD "90 dBA" equipment. Full-Load Operation Condition.

- No Aux Skid or other equipment skids included. VBV closed at full load.

- NOTE: This set of Data: All Positions 5' above base of Skid. Combustion Exhaust noise EXCLUDED.

MEAG	R-FIELD POSITIONS (ONE (1) UNIT OUTDOORS)			Octave	-Band	Center							
Positi		31	63	125	250	500	1K	2K	4K	8K	Lin.	A-Wt.	
	Actual Position Locations are ADJUSTABLE.			SPL's i	n dB re	20 Mic	ropasc	als		- 1	i		
	Location descriptions below indicate spreadsheet des	ign pos	sitions.							1			
	Lt. Side, 66' 7" from gen. end, 3' to side of package £	92	89	89	79	75	71	70	71	65	95	79.6	1
M-1:	A-Wt Levels:	53	63	73	70	72	71	71	72	64	ļ		
M.2-	Lt. Side, 52' 7"from gen. end, 3' to side of package	94	92	91	81	79	72	73	75	68	98	82.4	2
W-2.	A-Wt Levels:	55	66	75	72	76	72	74	76	67	l		
M-3:	Lt. Side, 30' 8.5" from gen, end, 3' to side of package	96	95	94	84	81	77	76	78	70	100	85.4	3
W-3.	A-Wt Levels:	57	69	78	75	78	77	77	79	69			
M-4.	Lt. Side, 6' 9" from gen. end, 3' to side of package	96	93	93	81	79	76	72	72	64	99	82.9	4
101	A-Wt Levels:	57	67	77	72	76	76	73	73	63	١		_
M-5:	Rt. Side, 6' 5" from gen. end, 3' to side of pkg.	96	93	93	81	79	76	72	72	64	99	83.0	5
	A-Wt Levels:	57	67	77	72	76	76	73	73	63			ے
M-6:	Rt. Side. 24' 3" from gen. end, 3' to side of pkg.	98	96	94	84	80	77	75	77	71	102	84.9	0
	A-Wt Levels:	59	70	78	75	77	77	76	78	70			7
M-7:	Rt. Side, 38' 2" from gen, end, 3' to side of pkg.	98	96	93	84	80	76	76	78	72	101	85.0	′
	A-Wt Levels:	59	70	77	75	77	76	77	79	71	98	83.4	۰
M-8:	Rt. Side, 58' 11" from gen. end, 3' to side of Pkg.	95	92	92	83	80	75	74	75	69 68	98	63.4	٥
	A-Wt Levels:	56	66	76	74	77	75	75	76	88			
	Number average over all positions:	96	93	92	82	79	75	73	75	68	99	83.2	
	Composite worst-case maximum:	98	96	94	84	81	77	76	78	72	102	85.6	
	S Nata Sanada	99	97	94	84	82	78	76	78	72	102	86.0	
SPL:	Expected Maximum, Not to Exceed:	33	٠.	• •							1		

86.0

Quantity of Turbine Generator Units:

1 Units

Correction Factor: 0.0 dB

FAR-FIELD POSITIONS at Distance:

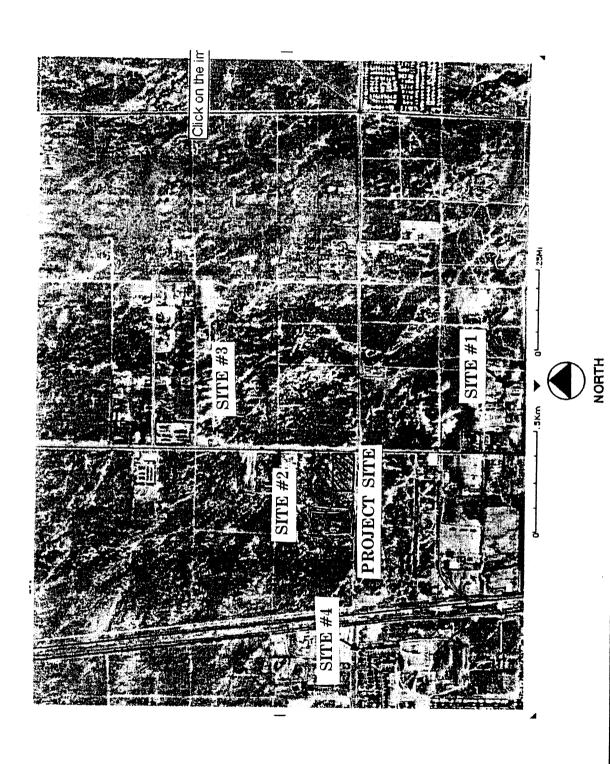
121.96 m.

Octave-Band Center Frequency (Hz) 400.0 Ft. Lin. A-Wt. Position dB re 20 Micropascals 53.8 F-1: Left Side (Cust. Connection Side) 52.5 F-2: Generator End 54.9 F-3: Right Side (Skids & Access Side) 53.7 F-4: Turbine Exhaust End 53.7 Number average over all positions: 54.9 Composite worst-case maximum:

NEAR-FIELD POSITIONS (UNIT INSIDE BUILDING):

Octave-Band Corrections, Inside Building (dB) For the corrections below, see ROOMCONST.XLS spreadsheet:
Octave-Band Correction (Penalty) for building:
4.1 2.6 Octave-Band Center Frequency (Hz) 125 250 500 1K 2K A-Wt. Position 81.3 M-1: Lt. Side, 86' 7" from gen. end, 3' to side of package E 74 74 76 77 79 80 74 75 74 75 78 79 79 80 77 83 80 80 77 74 A.Wt I evels: 84.1 2 74 85 76 83 74 83 74 85 78 M-2: Lt. Side, 52' 7"from gen, end, 3' to side of package 69 77 78 74 75 74 75 77 78 77 78 76 A-Wt Levels: 70 65 64 66 65 72 71 73 72 71 70 87.1 3 **6** 80 **7** 71 M-3: Lt. Side, 30' 8.5" from gen. end, 3' to side of package 78 A-Wt Leveis: 70 96 70 99 73 98 72 79 M-4: Lt. Side, 6' 9" from gen, end, 3' to side of package 78 A-Wt Levels: 78 82 79 82 79 81 78 79 96 80 95 79 Rt. Side, 6' 5" from gen, end, 3' to side of pkg. 78 78 77 77 76 A-WA I evels M-8: Rt. Side, 24' 3" from gen. end. 3' to side of pkg. A-Wt Levels: 86.7 7 Rt. Side, 38' 2" from gen. end, 3' to side of pkg. 76 77 A-Wt Levels: 85.1 8 78 75 Rt. Side, 58' 11" from gen. end, 3' to side of Pkg. 60 A-Wt Levels: 84.9 Number average over all positions: 87.3 Composite worst-case maximum:

Construction E	quipment Noise Levels at 50 Feet
	60 70 80 90 100 110
Compactors	
Front Loaders	
Backhoes	
Tractors	
Scrapers, Graders	
Pavers	
Trucks	
Concrete Mixers	
Concrete Pumps	
Cranes (Moveable)	
Cranes (Derrick)	[]
Pumps	
Generators	
Compressors	
Pneumatic Wrenches	
Jack Hammers & Rock Drills	
Pile Drivers (Peaks)	
Vibrators	
Saws	



		TOW	YARD	TRA	ILER	GRAPE			WALL
		Leo	LMAX	Lea	LMAX	Lea	Luux	Lea	Lux
May 01	11:00 AM	56.0	- 82.9						
	12:00 PM	47.8	63.1	64.5	95.9				
	01:00 PM	46.8	67.2	50.6	63.2				
	02:00 PM	50.1	59.8	54.6	69.0				
	03:00 PM	53.3	67.1	58.6	73.3				
	04:00 PM	57.2	69.6	64.3	75.8]
				66.9	81.7				
	05:00 PM	57.0	72.6						
	06:00 PM	58.0	72.3	66.4	77.9			 	
	07:00 PM	54.9	70.4	64.8	77.8				
	08:00 PM	49.1	62.7	60.5	77.0				
	09:00 PM	49.7	72.1	54.3	67.2				
	10:00 PM	48.4	61.8	51.5	67.6				
	11:00 PM	50.3	70.2	54.9	73.8				
	12:00 PM	48.4	67.3	51.6	67.8				
May 01	01:00 AM	49.9	66.1	53.6	67.6				
,,,d, 0.	02:00 AM	47.2	63.1	54.7	69.4				
			66.7	55.3	69.1				
	03:00 AM	49.9			74.8			l	
	04:00 AM	55.2	69.9	60.3		-			
	05:00 AM	54.8	68.9	65.6	79.6			 	
	06:00 AM	55.0	69.9	64.0	76.1				
	07:00 AM	57.1	73.6	67.0	79.0			 	<u> </u>
	08:00 AM	54.2	68.0	62.2	75.9				
	09:00 AM	47.1	58.8	55.1	72.3			ļ	
	10:00 AM	54.6	73.1	58.6	73.5			<u> </u>	
	11:00 AM	53.4	72.3	57.9	71.4				
	12:00 PM	47.6	62.0	53.8	66.3				
		49.1	63.4	53.2	64.7				
	01:00 PM		68.1	55.2	70.2			Ī	
	02:00 PM	49.6							
	03:00 PM	50.6	61.7	55.3	67.0			 	
	04:00 PM	50.7	68.0	55.3	68.3				
	05:00 PM	50.2	64.3	58.0	69.7			-	
	06:00 PM	50.9	73.7	54.6	70.7			<u> </u>	
	07:00 PM	44.5	65.5	52.1	69.7				
	08:00 PM	43.9	60.5	46.6	62.0				
	09:00 PM	43.8	62.2	49.8	64.6				
	10:00 PM	39.3	54.7	58.1	82.5				
	11:00 PM	39.3	55.9	54.0	76.6				
		37.6	50.3	47.8	62.6				
	12:00 PM			44.6	66.3	i			
May 01	01:00 AM	36.3	47.1					1	
	02:00 AM	37.2	49.2	59.1	89.7				
	03:00 AM	37.1	56.8	46.6	63.5				
	04:00 AM	38.7	65.3	39.4	56.3				
	05:00 AM	38.0	50.8	53.2	78.1			-	
	06:00 AM	41.3	55.5	48.7	62.8				
	07:00 AM	47.9	72.0	52.4	71.0				
	08:00 AM	51.1	66.5	49.9	67.5				
	09:00 AM	55.8	75.2	53.3	72.0				
		54.1	76.0	51.1	68.1				
	10:00 AM		 		92.4				
	11:00 AM	64.1	80.3	65.7	32.4	54.3	76.4	67.6	67.6
	12:00 PM		-	-	+	54.7	69.1	66.7	66.7
	01:00 PM		ļ	-				66.5	66.5
	02:00 PM			-		55.6	67.9		68.1
	03:00 PM				ļ	52.8	67.0	68.1	
	04:00 PM					44.5	62.1	67.7	67.7
	05:00 PM					43.7	63.7	65.4	65.4
	06:00 PM					40.3	57.6	63.0	63.0
	07:00 PM					39.5	53.0	62.2	62.2
	08:00 PM					47.3	69.8	62.1	62.1
	09:00 PM			1		38.0	59.7	62.3	62.3
			+	 	+	39.8	60.4	59.4	59.4
	10:00 PM		+	+		39.3	52.9	58.5	58.5
	11:00 PM			+	+	37.9	51.1	59.3	59.3
	12:00 PM	ļ			+		61.9	53.9	53.9
May 01	01:00 AM				+	47.3			55.1
	02:00 AM					47.2	70.0	55.1	
	03:00 AM					49.7	71.6	57.4	57.4
	04:00 AM					41.4	63.2	60.4	60.4
	05:00 AM					47.7	60.6	65.1	65.1
	06:00 AM		-			48.7	67.9	66.6	66.6
	07:00 AM					54.4	74.2	67.1	67.1
				+	1	48.9	66.7	64.9	64.9
	08:00 AM				+	44.2	68.9	63.8	63.8
	09:00 AM		-				66.2	64.4	64.4
	10:00 AM					45.2		65.1	65.1
	11:00 AM	<u> </u>				44.2	61.2		63.6
	12:00 PM	1		1	1	47.3	66.8	63.6	

MONITORING RESULTS FROM FOUR MONITORING LOCATIONS (2 PAGES)

	01:00 PM		51.8	77.1	64.8	64.8
	02:00 PM		49.8	68.7	65.5	65.5
	03:00 PM		50.7	64.8	67.8	67.8
	04:00 PM		54.4	74.9	67.0	67.0
	05:00 PM		51.5	69.8	66.0	66.0
	06:00 PM		53.3	66.6	65.1	65.1
	07:00 PM		51.2	67.3	64.1	64.1
	08:00 PM		48.0	68.8	62.7	62.7
	09:00 PM		43.2	54.9	61.3	61.3
	10:00 PM		43.5	61.7	60.4	60.4
	11:00 PM				59.0	59.0
	12:00 PM				57.0	57.0
5 May 01	01:00 AM				53.4	53.4
	02:00 AM				54.3	54.3
	03:00 AM				53.7	53.7
	04:00 AM				57.7	57.7
	05:00 AM				61.4	61.4
	06:00 AM				61.9	61.9
	07:00 AM				62.6	62.6
	08:00 AM				63.8	63.8
	09:00 AM				63.5	63.5
	10:00 AM				64.2	64.2
	11:00 AM				64.4	64.4
	12:00 PM I				62.9	62.9
	01:00 PM				63.5	63.5
	02:00 PM				64.6	64.6
	03:00 PM				64.2	64.2
	04:00 PM				64.7	64.7
	05:00 PM		į		64.3	64.3
	06:00 PM				61.7	61.7
	07:00 PM				62.2	62.2
	08:00 PM				62.1	62.1
	09:00 PM				60.3	60.3
	10:00 PM				60.2	60.2
	11:00 PM				57.7	57.7
	12:00 PM				56.1	56.1
6 May 01	01:00 AM				57.1	57.1
	02:00 AM				53.4	53.4
	03:00 AM				52.7	52.7
	04:00 AM				50.6	50.6
	05:00 AM				56.5	56.5
	06:00 AM				59.2	59.2
	07:00 AM				60.5	60.5
	08:00 AM				63.0	63.0
	09:00 AM				64.6	64.6
	10:00 AM				63.5	63.5
	11:00 AM				62.0	62.0
	12:00 PM				63.7	63.7
	01:00 PM				63.3	63.3
	02:00 PM			~	62.5	62.5
	03:00 PM				61.8	61.8
	04:00 PM				61.8	61.8

Sound 32 Data and Results

	Traffic li	aformation	
Roadway Name	Speed Limit	Current ADT (average daily trips)	Projected ADT (average daily trips)
Avenue H	45 mph	1,700 ADT	7,900 ADT

		Traffic (Conditions			
Roadway Name	Condition	Total %	Cars	Medium Trucks	Heavy Trucks	
100adway 14ame	Condition	ADT	(hourly)	(hourly)	(hourly)	
	Current	100	98.5%	1.0%	0.5%	
Avenue H	Current	1700	97	0	0	
11vonue 11	_	100	98.5%	1.0%	0.5%	
	Future	7900	451	4	2	

Current Traffic Study

City of Lancaster Public Works Department Alan Perkins @ 661-723-6154 Avenue H (between Division Street and Sierra Highway)

Future Projected Traffic Study

City of Lancaster Public Works Department Alan Perkins @ 661-723-6154 Avenue H (between Division Street and Sierra Highway)

Sound 32 Raw Data for Caltrans Version of Stamina2/Optima

Future ADT Traffic Data to Produce Noise Contours

		*	* SOU	ND32 (CA	LTRANS	S VER	SION	OF ST	AMIN	A2/OPTIMA) * *		
BARRI DATE	ER C	OST FI	LE :	FUTURE.T CALIF\$.D 05-08-20	TA 01							=====	=====
====	====	=====	====	======	=====	====	=====						
TRAFF	ric D	ATA											
LANE NO.		AUT VPH	O MPH	MEDIUM VPH	TRKS MPH	Н	EAVY VPH	TRKS MPH	DES	CRIPTION			
1		451	 45	4	45	-	2	45	ave	nue h			
====	====	=====	=====	=======	=====			=====	====				
LANE													
LANE		GRADE COR.		x		Y		z		MENT CRIPTION			
1	1	NO		.000.0									
				Y		Z	DNI	L PEOI	PLE	ID			
1		0.0	•	22.0		5.0	67	7 50	00	R-1			
2 3		0.0		70.0 198.0		5.0	67	/ 50 7 50	00	R-2 R-3			
3		U.U EIVER				3.0							
	R-2 R-3		60.										
						====	=====	=====	====	========		:=====	=====
====:	====	=====											
		RATES											
ALL	LANE	/RECEI	/ER P.	AIRS =	3.0 DE	BA							
====	====	======	====	=======	=====	====	=====	3222 3	===	=======	======		:=====
K -	CONS'	TANTS											
ALL	LANE	RECEIV	VER/P	AIRS =	2.0	BA							
				======			====	====	====	=======	=====		

ı		1			Distance	400		T	ĭ		
	Level			8000		98	-1.1	35.1			
	ressure			4000		44	1	45.3			
	Sound P		(Hz.)	2000		44	1.2	45.4			
	SPL = Sound Pressure Level		equency	1000		45	0	44.9			
	و		enter Fr	500		48	-3.2	44.5			
	200.0 Sw _L = Sound Power Level		Octave Band Center Frequency (Hz.)	250		53	9.8-	44.7			***************************************
	ound Po		<u>Octave</u>	125		<i>L</i> 9	-16.1	51.2			***************************************
	SwL = S			63		29	-26.2	40.7			***************************************
	200.0			31.5		7.1	-39.4	31.2	54.8	6.09	
	Evaluated Distance					Right Side S _{PL} (A)	A-Weight	Octave Sum	Overall SpL(A)	Calculated SpL(A)	

- - - - - - -	5.5	2.5	1.1	-30.5	0.9		
	-	-	 	-	\vdash		
134	45.5	88.5	-	-27.7	61.8		
138	45.5	92.5	1.2	-24.8	6.89		
140	45.5	94.5	0	-21.9	72.6		
142	45.5	96.5	-3.2	-19	74.3		
143	45.5	97.5	9.8-	-16.1	72.8		
141	45.5	95.5	-16.1	-13.3	66.1		
139	45.5	93.5	-26.2	-10.4	26.9		
137	45.5	91.5	-39.4	-7.5	44.6	78.9	
Turbine Exhaust Swl	$S_{PL} = S_{WL} + 20 Log r5$	S _{PL} / Distance	A-Weight	Exhst Sil D.I.L.	Octave Sum	Calculated Spr(A)	

38	5.5	2.5		-17.4	4.0	
	4	6		-1	12	
138	45.5	92.5	1	-32.4	61.1	
138	45.5	92.5	1.2	-44.4	49.3	
136	45.5	90.5	0	-44.4	46.1	
125	45.5	79.5	-3.2	-34	42.3	
121	45.5	75.5	9.8-	-20	46.9	
122	45.5	2.92	-16.1	-13	47.4	
129	45.5	83.5	-26.2	-10	47.3	
129	45.5	83.5	-39.4	9-	38.1	74.2
Turbine Intake Swr	$S_{PL} = S_{WL} + 20 \text{ Log r}5$	SPL / Distance	A-Weight	Intk Silencer D.I.L.	Octave Sum	Calculated Spr(A)

		400	Feet Rese	Distant	Distance																Calculated Spr At Negrost Postdones	Tresidelice	Teet.	(e) an		
evel	8000	36.2	-1-	25.1	00.1		1000	120.0	37.0	90.4	-1:1	868		1 90 0	138.0	35.1	102.9	-	101.8		Nagract	900 COS	100 F	200		
essure L	4000	44.3	1.0	15.3	40.0		1940	0.4.0	0.76	30.4	1.0	97.4		190.0	0.001	35.1	102.9	1.0	103.9	٠.	Spr At	onerty.	Oper cy Noise	2		
SPL = Sound Pressure Level equency (Hz.)	2000	44.2	1.2	45.4	10.1		1400 1380 1940 1950	97.6	0.10	100.4	1.2	101.6		138.0	100.0	55.1	102.9	1.2	104.1		alculated	Distance to Property	Single Unit Noise	0		
$\frac{\text{SPL} = S}{\text{equency}}$	1000	44.9	0.0	44.9			14001	37.6	1097	1077	0.0	102.4		136.0	95.1	99.1	100.9	0.0	100.9	*		Dista	S			
$\begin{array}{c c} Level & SPL = S \\ \hline Octave Band Center Frequency \\ \hline \end{array}$	500	47.7	-3.2	44.5		***************************************		37.6	104.4	9.0	7.0-	101.2	**********	125.0	9K 1	1.00	89.9	-3.2	2.98	**********		*****	****]		
e Band C	250	53.3	-8.6	44.7		*****	143.0	37.6	105.4	-8 G	0.0	96.8	**********	121.0	35.1	1.00	85.9	-8.6	77.3	* **********		Feet	Feet :	Feet	dR(A)	74.27
Sound Power Level	125	67.3	-16.1	51.2		******	141.0	37.6	103.4	-161	101	87.3	*****	122.0	35.1	1:00	80.9	-16.1	8.02	* *********	ine	80 I	80.0 F	60 F	107.6 d	
ound Pov	63	6.00	-26.2	40.7		* *******	139.0	37.6	101.4	292-	101	7.C/	* *********	129.0	35.1	0 60	35.3	7.97-	67.7	* *************************************	roperty Line	B(A) at	B(A) at	B(A) at	e Level	
	31.5	0.07	-39.4	31.2	54.8	***************************************	137.0	37.6	99.4	-39.4	000	00.00	* **********	129.0	35.1	0 60	30.3	-39.4	54.5	***************************************	(A) At Pr	68.8 dB(A) at	107.6 d]	109.0 d]	ne Noise	2 700 00 00 00
	Bight Gide Gar	ATT A TILE OF THE TAIL AND THE	A-Weight	Octave Sum	Overall $S_{PL}(A)$		Turbine Exhaust Swr	SPL = SwL + 20 Log r5	SPL / Distance	A-Weight	Ootorro Cum	Octave Sum	. I	`	$S_{PL} = S_{WL} + 20 Log r5$		OFL/ Distance	A-weignt	Octave Sum		Calculated Spr(A) At P	Turbine Body	Turbine Exhaust 107.6 dB(A) at	Turbine Intake 109.0 dB(A) at	Single Turbine Property Line Nois	S 14 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

85

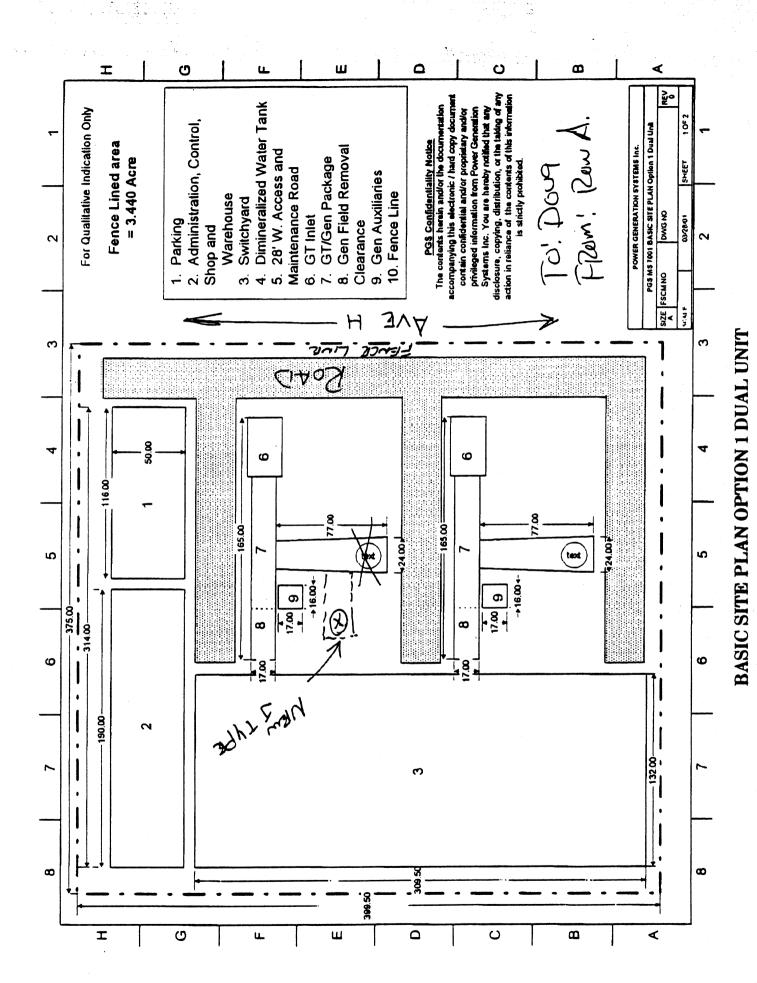
Swī	11	und Pov	Sound Power Level			$SPI_{r} = 0$	Sound Pr	Sound Pressure Level	evel	
1			Octave	Band C	Octave Band Center Frequency	equency	(Hz.)			
ွတ	31.5	63	125	250	200	1000	2000	4000	8000	
5	9.07	6.99	67.3	53.3	47.7	44.9	44.2	44.3	36.2	400
ကု	-39.4	-26.2	-16.1	9.8-	-3.2	0.0	1.2	1.0	-1.1	Feet Base
	31.2	40.7	51.2	44.7	44.5	44.9	45.4	45.3	35.1	Distance
. 🗻 🕶	54.8	***	******	******	***************************************	****	****	***	*****	
(3)	137.0	139.0	141.0	143.0	142.0	140.0	138.0	134.0	128.0	
	37.6	37.6	37.6	37.6	37.6	37.6	37.6	37.6	97.8	
	99.4	101.4	103.4	105.4	104.4	102.4	100.4	96.4	90.4	
	-10.7	-15.0	-19.3	-23.5	-27.8	-32.1	-36.4	-40.6	-44.9	
	-3.0	-4.0	-4.0	-4.0	-11.0	-11.0	-18.0	-18.0	-18.0	
	-1.0	-2.0	-3.0	-4.0	-5.0	0:9-	0.9-	-6.0	-5.0	
	-3.5	-4.3	-5.1	9.7-	9.7-	-7.0	-7.0	-5.9	-5.0	
	81.2	76.2	72.0	66.4	53.1	46.3	33.0	25.9	17.5	
9	2.98	81.7	77.7	77.7	79.7	2.67	79.7	79.7	1.67	
_	81.2	76.2	72.0	66.4	53.4	47.7	42.7	42.3	42.2	
03	-39.4	-26.2	-16.1	-8.6	-3.2	0.0	1.2	1.0	-1.1	
i	41.8	20.0	55.9	8.73	50.2	47.7	43.9	43.3	41.1	
	: [
×: 1	129.0	129.0	122.0	121.0	125.0	136.0	138.0	138.0	138.0	
	35.1	35.1	35.1	35.1	35.1	35.1	35.1	35.1	35.1	
	93.9	93.9	6.98	85.9	89.9	100.9	102.9	102.9	102.9	
	0.0	-2.0	-3.0	-4.0	-4.0	-5.0	-11.0	-17.0	-22.0	
	-7.0	-11.0	-15.0	-19.0	-36.0	-54.0	-55.0	-47.0	-27.0	
	-39.4	-26.2	-16.1	9.8-	-3.2	0.0	1.2	1.0	-1.1	
	47.5	54.7	52.8	54.3	46.7	41.9	38.1	39.9	52.8	
	************	**********	***********	**********	********	********	********	*************	**********	
	Calculated Spr.(A) At P	Property Line	Line				Calculate	d Spr. At	Nearest	Calculated Sp. At Nearest Residence
		TO (V) OF	00	15.00		֖֖֖֖֖֖֖֖֖֖֖֖֖֖֖֓	C of Comp		Č	70°E

Calc	istanc	Sing		
	Α			
	****	*****	*******	
	Feet	Feet .	Feet	$d\mathbf{B}(\mathbf{A})$
Line	08	80.0	- 60	69.5
operty.	dB(A) at	2 dB(A) at	B(A) at	oise Level
A) At Pr	8.89	61.2 d	60.	ine Nois
f)Tdg per	ne Body		ntake	perty Li
Calculat	Purbine	bine Ex	irbine Ir	ine Pro
	Ť.	Tur	To	gle Turb
				Sing

Calculated SPL At Nearest Residence
Distance to Property 200 Feet
Single Unit Noise 59.1 dB(A)

DOUGLAS EILAR & ASSOCIATES 321 N. WILLOWSPRING DRIVE ENCINITAS, CA 92024 • 760/753-1865 • FAX 760/753-0111 • DGEILAR AOL.COM

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<u> </u>	L		Distance	cc	,				
		. 0008		102.0	-1.1	-25.0	75.9		
ure Level		4000		108.0	1.0	-23.0	86.0		
und Press		[z.) 2000		116.0	1.2	-25.5	91.7		
SPL = Sound Pressure Level		Octave Band Center Frequency (Hz.) 25 550 500 1000		120.0	0.0	-28.0	92.0		
		Center Fre 500		120.0	-3.2	-34.0	82.8		
Power Level		ave Band 250		121.0	9.8-	-38.0	74.4		
- 177		: Oct 125		123.0	-16.1	-29.0	6.77		
SwL = Sc		63		124.0	-26.2	-19.0	78.8		dB(A)
350.0		81,5			-39.4	-15.0	49.6	95.9	54.5
Evaluated Distance 350.0 SwL = Sound		Blaokstart Generator		L7042GSI	A-Weight	Silencer Interpreted	Octave Sum	Overall Spl(A)	Calculated Spr (A)



49+:50 10 01 REW

